

Multifunctional Thermostatic Circulation Valve MTCV - Low lead





<u>Yantos</u>

Function



The MTCV - is a thermostatic self-acting, proportional valve. A thermo-element (*fig. 6 elem. 4*) is placed in the valve cone (*fig. 6 elem. 3*) to react to temperature changes.

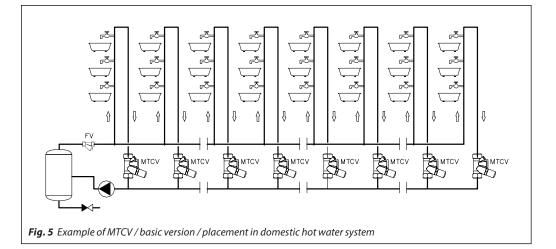
When increases the water temperature above the set point value, the thermo-element expands and the valve's cone moves towards the valve seat, thus limiting circulation flow. When decreases the water temperature below the set point value, the thermo-element will open the valve and allow more flow in the circulation pipe. The valve is in equilibrium (nominal flow = calculated flow) when the water temperature has reached the value set on the valve.

The MTCV regulating characteristic is shown in fig. 13, version A.

When the water temperature is 5 $^{\circ}$ C higher than the set point value, the flow through the valve stops.

A special sealing of the thermo-element protects it against direct contact with water, which prolongs the durability of the thermoelement and at the same time secures a precise regulation.

A safety spring (*fig. 6 elem. 6*) protects the thermo-element from being damaged when the water temperature exceeds the value on the set point.



Design

- 1. Valve body
- 2. Spring
- 3. Cone
- 4. Thermo-element
- 5. O-ring
- 6. Safety spring
- 7. Setting ring
- 8. Setting knob
- 9. Plug for covering the setting
- 10. Cone for disinfection module
- 11. Safety spring
- **12.** Plug for thermometer
- 13. Plug for disinfection module

Data sheet

Function



* thermometer is accessory

The MTCV standard version - A can easily and quickly be upgraded to the thermal disinfection function against the Legionella bacteria in hot water systems.

After removing the plug from the disinfection plug (*fig. 6 elem. 13*)-(this can be done during working conditions, under pressure) the thermostatic disinfection module can be mounted (*fig. 9 elem. 17*).

The disinfection module will control the flow according to its regulating characteristics, (*fig. 13, version B*) thus performing a thermal disinfection of the hot water installation.

The mounted disinfection module automatically opens a by-pass of Kv min = $0.15 \text{ m}^3/\text{h}$, which allows flow for the disinfection. In the A version of the MTCV this by-pass is always closed in order to avoid sedimentation of dirt and calcium. The MTCV can thus be upgraded with the disinfection module even after a long period of working in the A version without risking blocking the bypass.

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The regulation module in basic version A works within the temperature range 35-60 °C. When the temperature of the hot water increases above 65° C the disinfection process starts - meaning the flow through the main seat of the MTCV valve stops and the bypass opens for the "disinfection flow". The regulating function is now performed by the disinfection module, which opens the bypass when the temperature is above 65° C.

The disinfection process is performed until a temperature of 70 °C is reached. When the hot water temperature is increased further, the flow through the disinfection bypass is reduced (the process of thermal balancing of the installation during disinfection) and when reaching 75 °C the flow stops. This is to protect the hot water installation against corrosion and sedimentation of calcium as well as to lower the risk of scalding.

A thermometer can optionally be mounted in both version A and B in order to measure and control the temperature of the circulating hot water.

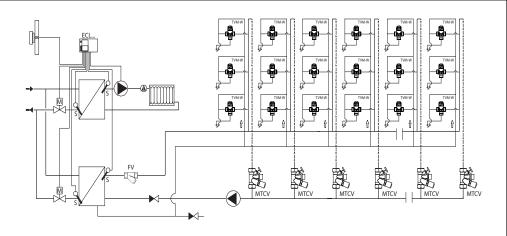


Fig. 8 Scheme of hot water installation with circulation - self acting version.

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Design

- 1-13 As described in fig. 6
- 14 Bypass for disinfection
- 15 Thermometer
- 16 Gasket Cu
- 17 Disinfecting module



Function

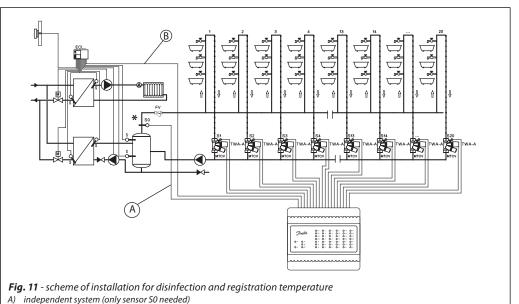


The MTCV version "A" and "B" can be upgraded to an electronic regulated disinfection process (version C).

After removing the disinfection plug (*fig. 6 elem. 13*) the adapter can be mounted (*fig. 12 elem. 21*) and the thermo actuator TWA can be mounted.

A temperature sensor PT 1000 has to be mounted in the thermometer head (*fig. 12 elem. 19*). Thermo-actuator and sensor are connected to the electronic regulator CCR2+ which allows an efficient and effective disinfection process in each circulation riser. The main regulation module works within the temperature range 35-60 °C. When the disinfection process/thermalwater treatment starts CCR2+ controls the flow through MTCV via thermo-actuators TWA. Benefits of an electronic regulated disinfection process with CCR2+ are:

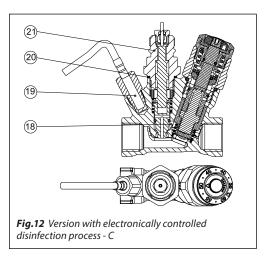
- Providing full control over the disinfection process in each individual riser.
- Optimisation of total disinfection time.
- Optional choice of temperature for the disinfection.
- Optional choice of time for the disinfection.
- On-line measurement and monitoring of the water temperature in each individual riser.
- Enabling the possibility of connecting to the controller in the heat substation or boiler room (i.e. Danfoss ECL) or to a BMS (Modbus).



B) dependent system (sensor S0 and connection to weather or another control needed)

Design

- 1-13 As described in fig. 6
- 18 Bypass; (position closed)
- 19 Temperature sensor PT 1000
- 20 Gasket Cu
- 21 Adapter to connect thermoactuator TWA



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Technical data

| Max. working pressure | 10 bar |
|---------------------------|----------|
| Test pressure | |
| Max. flow temperature | 100 °C |
| k _{vs} at 20 °C: | |
| - DN20 | 1.8 m³/h |
| - DN15 | 1.5 m³/h |
| Hysteresis | 1.5 K |

| Material of parts in contact with water: | |
|--|------|
| Valve body: Basic | |
| PURE (< 0.1 % lead) F | }g+ |
| Spring housing, etcCuphin alloy (CW72 | 4R) |
| O-rings EP | DM |
| Spring, bypass cones Stainless st | teel |
| ConePOM-C (Acetal Homopolyn | ner) |

Ordering

| Valve - basic version A | Code No. | Valve - PURE version A | Code No. |
|-------------------------|----------|------------------------|----------|
| DN 15 | 003Z4515 | DN 15 | 003Z6515 |
| DN 20 | 003Z4520 | DN 20 | 003Z6520 |

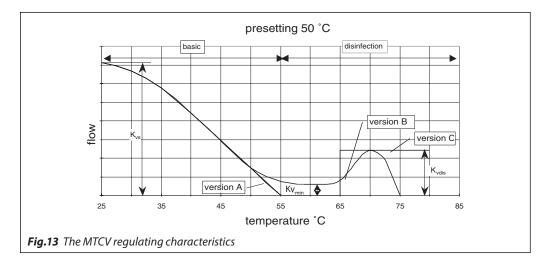
Accessories and spare parts

| Accessory | | Comments | Code No. |
|--|----------|-------------------------|----------|
| Thermostatic disinfection module - B | | DN 15/DN 20 | 003Z2021 |
| | | G ½ × Rp ½ | 003Z1037 |
| Fittings with shut-off ball valve (for allen key 5 mm), DN 20 | | G ¾ × Rp ¾ | 003Z1038 |
| Thermometer with adapter | | DN 15/DN 20 | 003Z1023 |
| Socket for ESMB PT1000 | | DN 15/DN 20 | 003Z1024 |
| Adapter for thermo-actuator | | DN 15/DN 20 | 003Z1022 |
| CCR2+ Controller | | see relevant data sheet | 003Z3851 |
| CCR+ Slave Unit | | see relevant data sheet | 003Z3852 |
| Temperature sensor ESMB Universal | | | 087B1184 |
| Temperature sensor ESMC contact | <u>_</u> | see relevant data sheet | 087N0011 |
| Fittings for soldering Cu 15 mm | | DN 15 | 003Z1034 |
| Fittings for soldering Cu 18 mm | | int. R 1/2" | 003Z1035 |
| Fittings for soldering Cu 22 mm | | DN 20 | 003Z1039 |
| Fittings for soldering Cu 28 mm | | int. R 3/4″ | 003Z1040 |
| Thermoactuator TWA-A/NC, 24V | | see relevant data sheet | 088H3110 |



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Regulating characteristics



- Basic version A
- Version B:

 $Kv_{min} = 0.15 \text{ m}^3/\text{h} - \text{min. flow through the bypass when main regulation module is closed.}$

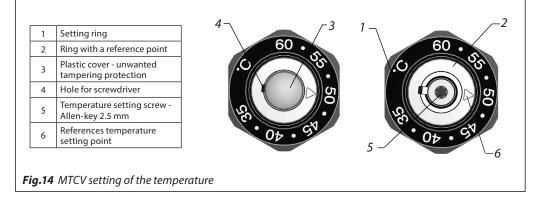
 $*Kv_{dis} = 0.60 \text{ m}^3/\text{h}$ for DN 20,

- *Kv_{dis} = 0.50 m³/h for DN 15 max. flow of the disinfection process by a temperature of 70 °C.
- Version C:

* $Kv_{dis} = 0.60 \text{ m}^3/\text{h}$ for DN 20 and DN 15 flow through the MTCV when the disinfection module is fully opened (regulation at thermo-actuator TWA-NC).

* Kv_{dis} - Kv during disinfection process

Main function setting



Temperature range: 35-60 °C MTCV's factory pre-setting 50 °C

The temperature setting can be made after removing the plastic cover (3), by lifting it with a screwdriver using the hole (4). The temperature setting screw (5) must be turned with an allenkey to match the wanted temperature on the scale with the reference point. The plastic cover (3) must be pressed back into place after the setting has been made. It is recommended to control the set temperature with a thermometer. The temperature of the hot water from the last tapping point on the riser must be measured*. The difference between the measured temperature at the last tapping point and the temperature set on the MTCV is due to heat losses in the circulation pipe between the MTCV and the tapping point.

* where TVM valves (thermostatic mixing valves) are installed the temperature must be measured before the TVM valve.

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Setting procedure

The required temperature setting of the MTCV depends on the required temperature at the last tap and the heat losses from the tap to MTCV in the same riser.

Example:

Required temperature at the last tap: 48 °C Heat losses from the last tap to the MTCV:

Required: correct setting of MTCV

Solution:

Correct setting of MTCV: 48 - 3 = 45 °C

Note:

3 K

After new setting use the thermometer to check if the required temperature at the tap is reached and correct the MTCV setting accordingly.

Pressure and flow chart MTCV - DN 15

Differential pressure 1 bar, DN 15

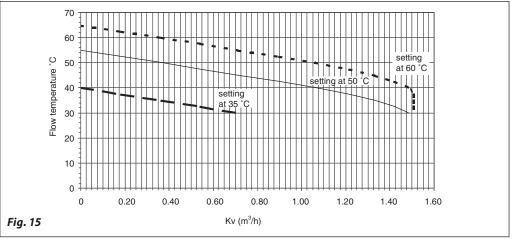
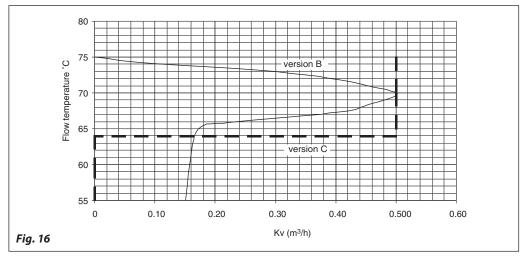


Table 1

| | preset | preset | preset | preset | preset | preset | kv |
|-------------|--------|--------|--------|--------|--------|--------|--------|
| | 60 °C | 55 °C | 50 °C | 45 °C | 40 °C | 35 °C | (m³/h) |
| | 65 | 60 | 55 | 50 | 45 | 40 | 0 |
| | 62.5 | 57.5 | 52.5 | 47.5 | 42.5 | 37.5 | 0.238 |
| | 60 | 55 | 50 | 45 | 40 | 35 | 0.427 |
| U | 57.5 | 52.5 | 47.5 | 42.5 | 37.5 | 32.5 | 0.632 |
| e | 55 | 50 | 45 | 40 | 35 | 30 | 0.795 |
| temperature | 52.5 | 47.5 | 42.5 | 37.5 | 32.5 | | 0.963 |
| ra | 50 | 45 | 40 | 35 | 30 | | 1.087 |
| be | 47.5 | 42.5 | 37.5 | 32.5 | | | 1.202 |
| E | 45 | 40 | 35 | 30 | | | 1.283 |
| vte | 42.5 | 37.5 | 32.5 | | | | 1.351 |
| Flow | 40 | 35 | 30 | | | | 1.394 |
| Ē | 37.5 | 32.5 | | | | | 1.437 |
| | 35 | 30 | | | | | 1.469 |
| | 32.5 | | | | | | 1.500 |
| | 30 | | | | | | 1.500 |

Differential pressure 1 bar, DN 15 - disinfection process



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Pressure and flow chart MTCV - DN 20

Differential pressure 1 bar, DN 20

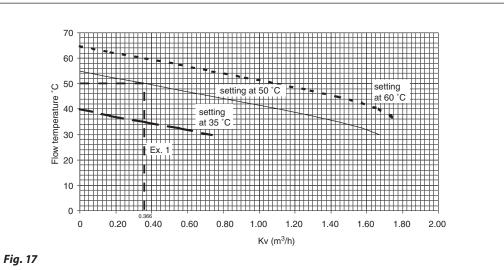
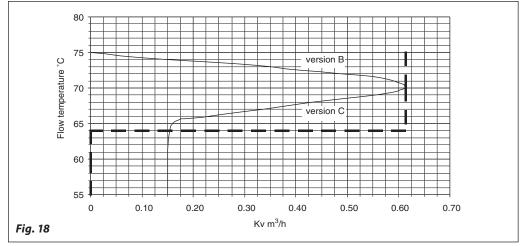


Table 2

| | preset | preset | preset | preset | preset | preset | kv |
|-------------|--------|--------|--------|--------|--------|--------|--------|
| | 60 °C | 55 °C | 50 °C | 45 °C | 40 °C | 35 °C | (m³/h) |
| | 65 | 60 | 55 | 50 | 45 | 40 | 0 |
| | 62.5 | 57.5 | 52.5 | 47.5 | 42.5 | 37.5 | 0.251 |
| | 60 | 55 | 50 | 45 | 40 | 35 | 0.442 |
| ν | 57.5 | 52.5 | 47.5 | 42.5 | 37.5 | 32.5 | 0.645 |
| | 55 | 50 | 45 | 40 | 35 | 30 | 0.828 |
| 1 | 52.5 | 47.5 | 42.5 | 37.5 | 32.5 | | 1.000 |
| Ta | 50 | 45 | 40 | 35 | 30 | | 1.164 |
| temperature | 47.5 | 42.5 | 37.5 | 32.5 | | 1 | 1.322 |
| 2 | 45 | 40 | 35 | 30 |] | | 1.462 |
| | 42.5 | 37.5 | 32.5 | | | | 1.577 |
| Flow | 40 | 35 | 30 | | | | 1.667 |
| Ē | 37.5 | 32.5 | | | | | 1.733 |
| | 35 | 30 | | | | | 1.753 |
| | 32.5 | | | | | | 1.761 |
| | 30 | | | | | | 1.761 |

Differential pressure 1 bar, DN 20 - disinfection process



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Example of calculation

Example:

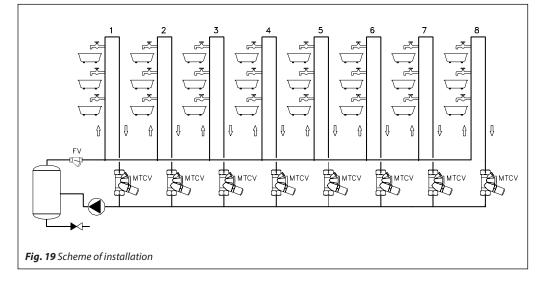
The calculation is done for a 3-storey building with 8 risers.

The following assumptions were used in order to simplify calculation: • Heat losses per meter of the pipe, $q_1 = 10 W/m *$

* during calculation it is required to calculate heat losses according to the country-specific standards.

Usually the calculated heat loses are dependent on:

- The dimension of the pipe
- The materials used in insulations
- The ambient temperature where the pipe is located
- The efficiency and condition of insulation
- Inlet of hot water temperature, $T_{sup} = 55 \text{ °C}$ •
- Temperature drop through the system, ΔT = 5 K
- Distance between risers, L = 10 m •
- Height of the risers, I = 10 m
- Installation scheme as shown below: •



I Basic operation

Calculation:

- calculation of heat losses in each riser (Qr) and header (Qh) Qr = I riser x q = (10 + 10) x 10 = 200 W
 - Qh = I horiz. x q = 10 x 10 = 100 W
- The table 3 shows the results of the • calculations:

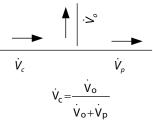


Table 3

| | | | heat losses | | | | | | | | | | | |
|-------|-----------|-----------|--------------------|----------|---------------|-------------------|------------|-----|------|------|-----|---------|------|------|
| riser | In risers | In header | Total in each part | ΣQ total | Factor risers | Flow in each part | Total flow | | | | | | | |
| | Qr (W) | Qh (W) | (W) | (W) | Factorrisers | Vo (l/h) | Vc (l /h) | | | | | | | |
| 1 | | | | 2400 | - | 36 | 412 | | | | | | | |
| 2 | | 100 | 100 | 100 | 100 | 100 | | | 2100 | 0.09 | 38 | 376 | | |
| 3 | | | | | | | | | 1800 | 0.1 | 40 | 339 | | |
| 4 | 200 | | | | | | 100 | 100 | 100 | 100 | 200 | 100 200 | 1500 | 0.12 |
| 5 | 200 | | | | 300 | 1200 | 0.14 | 47 | 256 | | | | | |
| 6 | | | | 900 | 0.18 | 52 | 210 | | | | | | | |
| 7 | | | 600 | | 0.25 | 63 | 157 | | | | | | | |
| 8 | | | | 300 | 0.4 | 94 | 94 | | | | | | | |

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Example of calculation *(continuous)*

• The total flow in the hot water circulation system is calculated using formula:

$$\dot{V} = \frac{\sum Q}{r \quad c_w \quad \Delta t_{hw}}$$

 $\Sigma Q\,$ - total heat loses in installation, (kW)

thus:
$$\dot{V}_{C}^{total} = ----$$

$$\frac{1}{2} = \frac{2.4}{1 \times 4.18 \times 5}$$

$$= 0.114 |/s = 412 |/h$$

The total flow in hot water circulation system is: 412 l/h - the circulation pump shall be sized for this flow.

• The flow in each riser is calculated using formula:

Flow in the riser number 1:

$$\dot{V}_{o} = \dot{V}_{c} \times \frac{Q_{o}}{Q_{o} + Q_{p}}$$

thus:

$$\dot{V}_0^1 = 412 \times \frac{200}{200 + 2100}$$

= 35.84 l/h \cong 36 l/h

Flow in remaining risers should be calculated in the same way.

- The pressure drop in the system Following assumptions were made to simplify calculation:
 - Linear pressure drop, $p_1 = 60 \text{ Pa/m}$ (Linear pressure is the same for all pipes)
 - Local pressure drop is equal to 33 % of total linear pressure drop, $p_r = 0.33 p_1$

thus:

- $p_{\rm r}$ = 0.33 \times 60 = 19.8 Pa/m \cong 20 Pa/m For the calculation used
- $p_{\text{basic}} = p_r + p_l = 60 + 20 = 80 \text{ Pa/m}$ - Local pressure drop across the MTCV is

calculated on the basis of:

Table 4

 $\Delta p_{_{MTCV}} = \left(\frac{0.01 \times \dot{V}_0}{Kv}\right)^2$

where: Kv - according to fig. 19 page 10

in this case

- $Kv = 0.366 \text{ m}^3/\text{h}$ for preset 50 °C
- \dot{V}_0 flow through the MTCV at the flow

temperature 50 °C (l/h)

• When designed flow have been calculated, use the fig. 17 on page 9.

Please note:

during pressure drop calculation across the valve the temperature of circulation water has to be observed. MTCV - Multifunction Thermostatic Circulation Valve has variable Kv value which is dependent on two values: the preset temperature and the temperature of the flow temperature.

When the $\dot{v}_{\rm o}$ and Kv are known, the pressure drop across MTCV is calculated using the following formula:

$$\Delta p_{MTCV} = \left(\frac{0.01 \times \dot{V}_0}{Kv}\right)^2$$

thus:

4

$$\Delta p_{MTCV} = \left(\frac{0.01 \times 94}{0.366}\right)^2 = 6.59 \, \text{kPa}$$

 $\Delta p_{MTCV} = (0.01 \times 94 / 0.366)^2 = 6.59 \text{ kPa}$

• Differential pressure across the pump:

$${}^*p_{pump} = \Delta p_{circuit} + \Delta p_{MTCV}$$
$$= 14.4 + 6.59 = 21 \text{ kPa}$$

Where:

- $\Delta p_{circuit}$ pressure drop in critical circuit (table 4)
- *p_{pump} includes pressure drop across all devices in circulation installation like: boiler, strainer etc.

| | pressure drop | | | acro | oss the MTCV | Total pressure |
|-------|---------------------------|--------------------|--------------------------------------|------------------|-------------------------------|----------------------|
| riser | In risers (kPa) | In header (kPa) | P _{circuit} (kPa) | V₀-flow (l/h) | ΔmMTCV pressure drop (kPa) | pump (kPa) |
| 1 | | | 14.4 | 36 | 0.97 | |
| 2 | | | 12.8 | 38 | 1.07 | |
| 3 | 1.6 | 1.6 | 11.2 | 40 | 1.19 | |
| 4 | | | 9.6 | 43 | 1.38 | |
| 5 | 1.6 | 1.6 | 8.0 | 47 | 1.64 | 21 |
| 6 | | | 6.4 | 52 | 2.01 | |
| 7 | | | 4.8 | 63 | 2.96 | |
| 8 | | | 3.2 | 94 | 6.59 | |

| Example of | calculation |
|--------------|-------------|
| (continuous) | |

II Disinfection

The heat losses and pressure drop should be calculated according to new conditions.

- inlet hot water temperature during disinfection $T_{dis} = 70 \text{ °C}$
- ambient temperature *T_{amb} = 20 °C (*T_{amb} - according to standard and norm obligatory)
- 1. The heat losses are calculated from the formula:

| $q_1 = K_j \times I \times \Delta T_1$ | \rightarrow | $K_j \times I = q_1 / \Delta T_1$ |
|--|---------------|-----------------------------------|
| | | for basic process |

$$q_2 = K_1 \times I \times \Delta T_2 \rightarrow K_1 \times I = q_2 / \Delta T_2$$

for disinfection process Thus :

$$q_2 = q_1 \frac{\Delta T_2}{\Delta T_1} = q_1 \left(\frac{T_{dis} - T_{amb}}{T_{sup} - T_{amb}} \right)$$

for given case:

$$q_2 = 10 (W/m) \left(\frac{70 \circ C - 20 \circ C}{55 \circ C - 20 \circ C} \right) = 14.3 W/m$$

In this case during disinfection process heat losses increase for around 43 %.

2. Required flow

Due to sequence disinfection process (step by step) only critical circuit should be calculated.

For given case:

$$\begin{array}{l} Q_{dis} = Q_{r} + Q_{h} \\ Q_{dis} = ((10 + 10) + (8 \times 10)) \times 14.3 \text{ W/m} = \\ 1430 \text{ W} = 1.43 \text{ kW} \end{array}$$

The flow:

$$\dot{V}_{dis} = \frac{1.43}{4.18 \times 5} = 0.0684 \, l/s = 246 \, l/h$$

3. The required pressure The required pressure during the disinfection process should be checked

 $p_{dispump} = p_{dis(circuit)} + \Delta p_{MTCV}$ where:

$$\Delta p_{\rm MTCV} = \left(\frac{0.01 \times \dot{V}_0}{Kv}\right)^2$$

Table 5

thus:

$$\Delta p_{\text{MTCV}} = \left(\frac{0.01 \times 246}{0.6}\right)^2 = 16.81 \text{kPa}$$

Due to lower flow comparing to basic condition (412 l/h), pressure drop in the installation, p_{circuit} should be recalculated.

$$\Delta p = \xi \frac{\rho w^2}{2}$$

where : w - velocity of the water (m/s)

By comparing conditions during basic operation and disinfection one can estimate:

$$p_{dis} = p_{basic} \times \frac{V_{dis}^2}{V_c^2}$$

where:

 $V_{\rm dis}$ - disinfection flow (l/h) $V_{\rm C}$ - basic flow (l/h)

Thus:

- for first part of installation

$$p_{dis}^1 = 80 \times \left(\frac{246}{412}\right)^2 = 29 Pa/m$$

This calculation should be done for all critical circuit. The table 5 shows the result of calculation.

For the critical circuit: $p_{dis(circuit)} = 0.57 + 0.68 + 0.84 + 1.08 + 1.48 \\ + 2.20 + 3.93 + 21.92 = 32.70 \ \text{kPa}$

The pump should be chosen to cover both requirements:

• basic operation, $\dot{V}_0 = 412 \text{ I/h}$ and $p_{pump} = 21 \text{ kPa}$

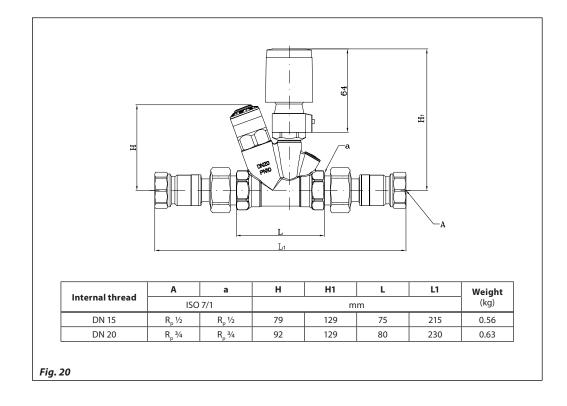
• disinfection operation \dot{V}_0 = 246 l/h and P_{pump}= 49.51 kPa

| Total pressure drop in critical circuit | pressure drop the circuit during disinfection process | | | | | | |
|--|---|--------|-------------------|--------------|-------|--|--|
| | pressure drop | length | new pressure drop | flow (l/h) | | | |
| in critical circuit | (kPa) | (m) | (Pa/m) | disinfection | basic | | |
| | 0.57 | | 29 | 246 | 412 | | |
| | 0.68 | | 34 | 246 | 376 | | |
| | 0.84 | 20 | 42 | 246 | 339 | | |
| 32.70 | 1.08 | | 54 | 246 | 299 | | |
| 52.70 | 1.48 | | 74 | 246 | 256 | | |
|] | 2.20 | | 110 | 246 | 210 | | |
| | 3.93 | | 196 | 246 | 157 | | |
| | 21.92 | 40 | 548 | 246 | 94 | | |
| | Σ 32.70 | | | | | | |





Dimensions



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